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SPECIFICATION

Ni-BASED SINGLE CRYSTAL SUPER ALLOY

TECHNICAL FIELD

The present invention relates to a Ni-based single crystal super alloy, and more particularly, to a technology employed for improving the creep characteristics of Ni-based single crystal super alloy.

BACKGROUND ART

An example of the typical composition of Ni-based single crystal super alloy developed for use as a material for moving and stationary blades subject to high temperatures such as those in aircraft and gas turbines is shown in Table 1.

Table 1

Alloy name	Elements (wt%)													
	Al	Ti	Ta	Nb	Mo	W	Re	C	Zr	Hf	Cr	Co	Ru	Ni
CMSX-2	6.0	1.0	6.0	-	1.0	8.0	-	-	-	-	8.0	5.0	-	Rem
CMSX-4	5.6	1.0	6.5	-	0.6	6.0	3.0	-	-	-	6.5	9.0	-	Rem
ReneN6	6.0	-	7.0	0.3	1.0	6.0	5.0	-	-	0.2	4.0	13.0	-	Rem
CMSX-10 K	5.7	0.3	8.4	0.1	0.4	5.5	6.3	-	-	0.03	2.3	3.3	-	Rem
3B	5.7	0.5	8.0	-	-	5.5	6.0	0.05	-	0.15	5.0	12.5	3.0	Rem

In the above-mentioned Ni-based single crystal super alloys, after performing solution treatment at a prescribed temperature, aging treatment is performed to obtain an Ni-based single crystal super alloy. This alloy is referred to as a so-called precipitation hardened alloy, and has a form in which the precipitation phase in the form of a γ' phase is precipitated in a matrix in the form of a γ phase.

Among the alloys listed in Table 1, CMSX-2 (Cannon-Muskegon, US Patent No. 4,582,548) is a first-generation alloy, CMSX-4 (Cannon-Muskegon, US Patent No. 4,643,782) is a

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second-generation alloy, ReneN6 (General Electric, US Patent No. 5,455,120) and CMSX-10K (Canon-Muskegon, US Patent No. 5,366,695) are third-generation alloys, and 3B (General Electric, US Patent No. 5,151,249) is a fourth-generation alloy.

Although the above-mentioned CMSX-2, which is a first-generation alloy, and CMSX-4, which is a second-generation alloy, have comparable creep strength at low temperatures, since a large amount of the eutectic γ' phase remains following high-temperature solution treatment, their creep strength is inferior to third-generation alloys.

In addition, although the third-generation alloys of ReneN6 and CMSX-10 are alloys designed to have improved creep strength at high temperatures in comparison with second-generation alloys, since the composite ratio of Re (5 wt% or more) exceeds the amount of Re that dissolves into the matrix (γ phase), the excess Re compounds with other elements and as a result, a so-called TCP (topologically close packed) phase precipitates at high temperatures causing the problem of decreased creep strength.

In addition, making the lattice constant of the precipitation phase (γ' phase) slightly smaller than the lattice constant of the matrix (γ phase) is effective in improving the creep strength of Ni-based single crystal super alloys. However, since the lattice constant of each phase fluctuates greatly fluctuated according to the composite ratios of the composite elements of the alloy, it is difficult to make fine adjustments in the lattice constant and as a result, there is the problem of considerable difficulty in improving creep strength.

In consideration of the above circumstances, the object of the present invention is to provide a Ni-based single crystal super alloy that makes it possible to improve strength by preventing precipitation of the TCP phase at high temperatures.

DISCLOSURE OF INVENTION

The following constitution is employed in the present invention in order to achieve the above object.

The Ni-based single crystal super alloy of the present invention is characterized by having a composition comprising 5.0-7.0 wt% of Al, 4.0-10.0 wt% of Ta, 1.1-4.5 wt% of Mo, 4.0-10.0 wt% of W, 3.1-8.0 wt% of Re, 0-0.50 wt% of Hf, 2.0-5.0 wt% of Cr, 0-9.9 wt% of Co and 4.1-14.0 wt%

of Ru in terms of its weight ratio, with the remainder consisting of Ni and unavoidable impurities.

In addition, the Ni-based single crystal super alloy of the present invention is characterized by having a composition comprising 5.0-7.0 wt% of Al, 4.0-6.0 wt% of Ta, 1.1-4.5 wt% of Mo, 4.0-10.0 wt% of W, 3.1-8.0 wt% of Re, 0-0.50 wt% of Hf, 2.0-5.0 wt% of Cr, 0-9.9 wt% of Co, and 4.1-14.0 wt% of Ru in terms of weight ratio, with the remainder consisting of Ni and unavoidable impurities.

In addition, the Ni-based single crystal super alloy of the present invention is characterized by having a composition comprising 5.0-7.0 wt% of Al, 4.0-6.0 wt% of Ta, 2.9-4.5 wt% of Mo, 4.0-10.0 wt% of W, 3.1-8.0 wt% of Re, 0-0.50 wt% of Hf, 2.0-5.0 wt% of Cr, 0-9.9 wt% of Co and 4.1-14.0 wt% of Ru in terms of weight ratio, with the remainder consisting of Ni and unavoidable impurities.

According to the above Ni-based single crystal super alloy, precipitation of the TCP phase, which causes a decrease in creep strength, during use at high temperatures is inhibited by the addition of Ru. In addition, by setting the composite ratios of other composite elements within their optimum ranges, the lattice constant of the matrix (γ phase) and the lattice constant of the precipitation phase (γ' phase) can be made to have optimum values. Consequently, strength at high temperatures can be enhanced. Furthermore, since the composition of Ru is 4.1-14.0 wt%, precipitation of the TCP phase, which causes a decrease in creep strength, during use at high temperatures, is inhibited.

In addition, the Ni-based single crystal super alloy of the present invention is preferably having a composition comprising 5.9 wt% of Al, 5.9 wt% of Ta, 3.9 wt% of Mo, 5.9 wt% of W, 4.9 wt% of Re, 0.10 wt% of Hf, 2.9 wt% of Cr, 5.9 wt% of Co and 5.0 wt% of Ru in terms of weight ratio, with the remainder consisting of Ni and unavoidable impurities, in the Ni-based single crystal super alloys previously described.

According to an Ni-based single crystal super alloy having this composition, the creep endurance temperature at 137 MPa and 1000 hours can be made to be 1344 K (1071°C).

In addition, the Ni-based single crystal super alloy of the present invention is preferably having a composition comprising 5.8 wt% of Co, 2.9 wt% of Cr, 3.1 wt% of Mo, 5.8 wt% of W, 5.8 wt% of Al, 5.6 wt% of Ta, 5.0 wt% of Ru, 4.9 wt% of Re and 0.10 wt% of Hf in terms of

weight ratio, with the remainder consisting of Ni and unavoidable impurities, in the Ni-based single crystal super alloys previously described.

According to an Ni-based single crystal super alloy having this composition, the creep endurance temperature at 137 MPa and 1000 hours can be made to be 1366 K (1093°C).

In addition, the Ni-based single crystal super alloy of the present invention is preferably having a composition comprising 5.8 wt% of Co, 2.9 wt% of Cr, 3.9 wt% of Mo, 5.8 wt% of W, 5.8 wt% of Al, 5.8 wt% (5.82 wt%) or 5.6 wt% of Ta, 6.0 wt% of Ru, 4.9 wt% of Re and 0.10 wt% of Hf in terms of weight ratio, with the remainder consisting of Ni and unavoidable impurities, in the Ni-based single crystal super alloys previously described.

According to an Ni-based single crystal super alloy having this composition, the creep endurance temperature at 137 MPa and 1000 hours can be made to be 1375 K (1102°C) or 1379 K (1106°C).

Furthermore, 0-2.0 wt% of Ti in terms of weight ratio can be included in the Ni-based single crystal super alloys previously described.

Furthermore, 0-4.0 wt% of Nb in terms of weight ratio can be included in the Ni-based single crystal super alloys previously described.

Furthermore, at least one of elements selected from B, C, Si, Y, La, Ce, V and Zr can be included in the Ni-based single crystal super alloys previously described.

In this case, it is preferable that 0.05 wt% or less of B, 0.15 wt% or less of C, 0.1 wt% or less of Si, 0.1 wt% or less of Y, 0.1 wt% or less of La, 0.1 wt% or less of Ce, 1 wt% or less of V and 0.1 wt% or less of Zr in terms of weight ratio are included in the alloys.

Furthermore, the above described Ni-based single crystal super alloy is more preferably having a composition comprising 5.0-7.0 wt% of Al, 4.0-10.0 wt% of Ta, 1.1-4.5 wt% of Mo, 4.0-10.0 wt% of W, 3.1-8.0 wt% of Re, 0-0.50 wt% of Hf, 2.0-5.0 wt% of Cr, 0-9.9 wt% of Co, 10.0-14.0 wt% of Ru, 4.0 wt% or less of Nb, 2.0 wt% or less of Ti, 0.05 wt% or less of B, 0.15 wt% or less of C, 0.1 wt% or less of Si, 0.1 wt% or less of Y, 0.1 wt% or less of La, 0.1 wt% or less of Ce, 1 wt% or less of V and 0.1 wt% or less of Zr.

Furthermore, the above described Ni-based single crystal super alloy is more preferably having a composition comprising 5.8-7.0 wt% of Al, 4.0-5.6 wt% of Ta, 3.3-4.5 wt% of Mo,

4.0-10.0 wt% of W, 3.1-8.0 wt% of Re, 0-0.50 wt% of Hf, 2.9-4.3 wt% of Cr, 0-9.9 wt% of Co, 4.1-14.0 wt% of Ru, 4.0 wt% or less of Nb, 2.0 wt% or less of Ti, 0.05 wt% or less of B, 0.15 wt% or less of C, 0.1 wt% or less of Si, 0.1 wt% or less of Y, 0.1 wt% or less of La, 0.1 wt% or less of Ce, 1 wt% or less of V and 0.1 wt% or less of Zr.

Furthermore, the above described Ni-based single crystal super alloy is more preferably having a composition comprising 5.0-7.0 wt% of Al, 4.0-10.0 wt% of Ta, 1.1-4.5 wt% of Mo, 4.0-10.0 wt% of W, 3.1-8.0 wt% of Re, 0-0.50 wt% of Hf, 2.9-5.0 wt% of Cr, 0-9.9 wt% of Co, 6.5-14.0 wt% of Ru, 4.0 wt% or less of Nb, 2.0 wt% or less of Ti, 0.05 wt% or less of B, 0.15 wt% or less of C, 0.1 wt% or less of Si, 0.1 wt% or less of Y, 0.1 wt% or less of La, 0.1 wt% or less of Ce, 1 wt% or less of V and 0.1 wt% or less of Zr.

Furthermore, the above described Ni-based single crystal super alloy is more preferably having a composition comprising 5.0-7.0 wt% of Al, 4.0-6.0 wt% of Ta, 3.3-4.5 wt% of Mo, 4.0-10.0 wt% of W, 3.1-8.0 wt% of Re, 0-0.50 wt% of Hf, 2.0-5.0 wt% of Cr, 0-9.9 wt% of Co, 4.1-14.0 wt% of Ru, 4.0 wt% or less of Nb, 2.0 wt% or less of Ti, 0.05 wt% or less of B, 0.15 wt% or less of C, 0.1 wt% or less of Si, 0.1 wt% or less of Y, 0.1 wt% or less of La, 0.1 wt% or less of Ce, 1 wt% or less of V and 0.1 wt% or less of Zr.

Furthermore, the above described Ni-based single crystal super alloy is more preferably having a composition comprising 5.0-7.0 wt% of Al, 4.0-5.6 wt% of Ta, 3.3-4.5 wt% of Mo, 4.0-10.0 wt% of W, 3.1-8.0 wt% of Re, 0-0.50 wt% of Hf, 2.0-5.0 wt% of Cr, 0-9.9 wt% of Co, 4.1-14.0 wt% of Ru, 4.0 wt% or less of Nb, 2.0 wt% or less of Ti, 0.05 wt% or less of B, 0.15 wt% or less of C, 0.1 wt% or less of Si, 0.1 wt% or less of Y, 0.1 wt% or less of La, 0.1 wt% or less of Ce, 1 wt% or less of V and 0.1 wt% or less of Zr.

Furthermore, the above described Ni-based single crystal super alloy is more preferably having a composition comprising 5.0-7.0 wt% of Al, 4.0-10.0 wt% of Ta, 3.1-4.5 wt% of Mo, 4.0-10.0 wt% of W, 3.1-8.0 wt% of Re, 0-0.50 wt% of Hf, 2.0-5.0 wt% of Cr, 0-9.9 wt% of Co, 4.1-14.0 wt% of Ru, 4.0 wt% or less of Nb, 0.05 wt% or less of B, 0.15 wt% or less of C, 0.1 wt% or less of Si, 0.1 wt% or less of Y, 0.1 wt% or less of La, 0.1 wt% or less of Ce, 1 wt% or less of V and 0.1 wt% or less of Zr.

Furthermore, the above described Ni-based single crystal super alloy is more preferably

having a composition comprising 5.8-7.0 wt% of Al, 4.0-10.0 wt% of Ta, 3.1-4.5 wt% of Mo, 4.0-10.0 wt% of W, 3.1-8.0 wt% of Re, 0-0.50 wt% of Hf, 2.0-5.0 wt% of Cr, 0-9.9 wt% of Co, 4.1-14.0 wt% of Ru, 4.0 wt% or less of Nb, 2.0 wt% or less of Ti, 0.05 wt% or less of B, 0.15 wt% or less of C, 0.1 wt% or less of Si, 0.1 wt% or less of Y, 0.1 wt% or less of La, 0.1 wt% or less of Ce, 1 wt% or less of V and 0.1 wt% or less of Zr.

Furthermore, the above described Ni-based single crystal super alloy is more preferably having a composition comprising 5.0-7.0 wt% of Al, 4.0-10.0 wt% of Ta, 3.1-4.5 wt% of Mo, 4.0-10.0 wt% of W, 3.1-8.0 wt% of Re, 0-0.50 wt% of Hf, 2.9-4.3 wt% of Cr, 0-9.9 wt% of Co, 4.1-14.0 wt% of Ru, 4.0 wt% or less of Nb, 2.0 wt% or less of Ti, 0.05 wt% or less of B, 0.15 wt% or less of C, 0.1 wt% or less of Si, 0.1 wt% or less of Y, 0.1 wt% or less of La, 0.1 wt% or less of Ce, 1 wt% or less of V and 0.1 wt% or less of Zr.

In addition, the above described Ni-based single crystal super alloy is more preferably having a composition comprising 5.0-7.0 wt% of Al, 4.0-10.0 wt% of Ta+Nb+Ti, 3.3-4.5 wt% of Mo, 4.0-10.0 wt% of W, 3.1-8.0 wt% of Re, 0-0.50 wt% of Hf, 2.0-5.0 wt% of Cr, 0-9.9 wt% of Co, 4.1-14.0 wt% of Ru, 0.05 wt% or less of B, 0.15 wt% or less of C, 0.1 wt% or less of Si, 0.1 wt% or less of Y, 0.1 wt% or less of La, 0.1 wt% or less of Ce, 1 wt% or less of V and 0.1 wt% or less of Zr.

Moreover, the Ni-based single crystal super alloy of the present invention is characterized by $a_2 \leq 0.999a_1$ when the lattice constant of the matrix is taken to be a_1 and the lattice constant of the precipitation phase is taken to be a_2 in the Ni-based single crystal super alloys previously described.

According to this Ni-based single crystal super alloy, the relationship between a_1 and a_2 is such that $a_2 \leq 0.999a_1$ when the lattice constant of the matrix is taken to be a_1 and the lattice constant of the precipitation phase is taken to be a_2 , and since the lattice constant a_2 of the precipitation phase is -0.1% or less of the lattice constant a_1 of the matrix, the precipitation phase that precipitates in the matrix precipitates so as to extend continuously in the direction perpendicular to the direction of the load. As a result, strength at high temperatures can be enhanced without dislocation defects moving within the alloy structure under stress.

In this case, it is more preferable that the lattice constant of the crystals of the precipitation phase a_2 is 0.9965 or less of the lattice constant of the crystals of the matrix a_1 .

Furthermore, the Ni-based single crystal super alloy of the present invention is characterized by comprising the feature that the dislocation space of the alloy is 40 nm or less.

BRIEF DESCRIPTION OF DRAWINGS

FIG. 1 is a diagram showing a relationship between change of lattice misfit of the alloy and creep rupture life of the alloy.

FIG. 2 is a diagram showing a relationship between dislocation space of the alloy and creep rupture life of the alloy.

FIG. 3 is a transmission electron microgram of the Ni-based single crystal super alloy showing an embodiment of the dislocation networks and dislocation space of the Ni-based single crystal super alloy of the present invention.

BEST MODE FOR CARRYING OUT THE INVENTION

The following provides a detailed explanation for carrying out the present invention.

The Ni-based single crystal super alloy of the present invention is an alloy comprised of Al, Ta, Mo, W, Re, Hf, Cr, Co, Ru, Ni (remainder) and unavoidable impurities.

The above Ni-based single crystal super alloy is an alloy having a composition comprising 5.0-7.0 wt% of Al, 4.0-10.0 wt% of Ta, 1.1-4.5 wt% of Mo, 4.0-10.0 wt% of W, 3.1-8.0 wt% of Re, 0-0.50 wt% of Hf, 2.0-5.0 wt% of Cr, 0-9.9 wt% of Co and 4.1-14.0 wt% of Ru, with the remainder consisting of Ni and unavoidable impurities.

In addition, the above Ni-based single crystal super alloy is an alloy having a composition comprising 5.0-7.0 wt% of Al, 4.0-6.0 wt% of Ta, 1.1-4.5 wt% of Mo, 4.0-10.0 wt% of W, 3.1-8.0 wt% of Re, 0-0.50 wt% of Hf, 2.0-5.0 wt% of Cr, 0-9.9 wt% of Co and 4.1-14.0 wt% of Ru, with the remainder consisting of Ni and unavoidable impurities.

Moreover, the above Ni-based single crystal super alloy is an alloy having a composition comprising 5.0-7.0 wt% of Al, 4.0-6.0 wt% of Ta, 2.9-4.5 wt% of Mo, 4.0-10.0 wt% of W, 3.1-8.0 wt% of Re, 0-0.50 wt% of Hf, 2.0-5.0 wt% of Cr, 0-9.9 wt% of Co and 4.1-14.0 wt% of Ru, with the remainder consisting of Ni and unavoidable impurities.

All of the above alloys have an austenite phase in the form of a γ phase (matrix) and an

intermediate regular phase in the form of a γ' phase (precipitation phase) that is dispersed and precipitated in the matrix. The γ' phase is mainly composed of an intermetallic compound represented by Ni_3Al , and the strength of the Ni-based single crystal super alloy at high temperatures is improved by this γ' phase.

Cr is an element that has superior oxidation resistance and improves the high-temperature corrosion resistance of the Ni-based single crystal super alloy. The composite ratio of Cr is preferably within the range of 2.0 wt% or more to 5.0 wt% or less, and more preferably 2.9 wt%. This ratio is more preferably within the range of 2.9 wt% or more to 5.0 wt% or less, more preferably within the range of 2.9 wt% or more to 4.3 wt% or less, and most preferably 2.9 wt%. If the composite ratio of Cr is less than 2.0 wt%, the desired high-temperature corrosion resistance cannot be secured, thereby making this undesirable. If the composite ratio of Cr exceeds 5.0 wt%, in addition to precipitation of the γ' phase being inhibited, harmful phases such as a σ phase or μ phase form that cause a decrease in strength at high temperatures, thereby making this undesirable.

In addition to improving strength at high temperatures by dissolving into the matrix in the form of the γ phase in the presence of W and Ta, Mo also improves strength at high temperatures due to precipitation hardening. Furthermore, Mo also improves the aftermentioned lattice misfit and dislocation networks of the alloy which relate characteristics of this alloy.

The composite ratio of Mo is preferably within the range of 1.1 wt% or more to 4.5 wt% or less, more preferably within the range of 2.9 wt% or more to 4.5 wt% or less. This ratio is more preferably within the range of 3.1 wt% or more to 4.5 wt% or less, more preferably within the range of 3.3 wt% or more to 4.5 wt% or less, and most preferably 3.1 wt% or 3.9 wt%. If the composite ratio of Mo is less than 1.1 wt%, strength at high temperatures cannot be maintained at the desired level, thereby making this undesirable. If the composite ratio of Mo exceeds 4.5 wt%, strength at high temperatures decreases, and corrosion resistance at high temperatures also decreases, thereby making this undesirable.

W improves strength at high temperatures due to the actions of solution hardening and precipitation hardening in the presence of Mo and Ta as previously mentioned. The composite ratio of W is preferably within the range of 4.0 wt% or more to 10.0 wt% or less, and most preferably 5.9 wt% or 5.8 wt%. If the composite ratio of W is less than 4.0 wt%, strength at high

temperatures cannot be maintained at the desired level, thereby making this undesirable. If the composite ratio of W exceeds 10.0 wt%, high-temperature corrosion resistance decreases, thereby making this undesirable.

Ta improves strength at high temperatures due to the actions of solution hardening and precipitation hardening in the presence of Mo and W as previously mentioned, and also improves strength at high temperatures as a result of a portion of the Ta undergoing precipitation hardening relative to the γ phase. The composite ratio of Ta is preferably within the range of 4.0 wt% or more to 10.0 wt% or less, more preferably within the range of 4.0 wt% or more to 6.0 wt% or less. This ratio is more preferably within the range of 4.0 wt% or more to 5.6 wt% or less, and most preferably 5.6 wt% or 5.82 wt%. If the composite ratio of Ta is less than 4.0 wt%, strength at high temperatures cannot be maintained at the desired level, thereby making this undesirable. If the composite ratio of Ta exceeds 10.0 wt%, the σ phase and μ phase form that cause a decrease in strength at high temperatures, thereby making this undesirable.

Al improves strength at high temperatures by compounding with Ni to form an intermetallic compound represented by Ni_3Al , which composes the γ phase that finely and uniformly disperses and precipitates in the matrix, at a ratio of 60-70% in terms of volume percent. The composite ratio of Al is preferably within the range of 5.0 wt% or more to 7.0 wt% or less. This ratio is more preferably within the range of 5.8 wt% or more to 7.0 wt% or less, and most preferably 5.9 wt% or 5.8 wt%. If the composite ratio of Al is less than 5.0 wt%, the precipitated amount of the γ phase becomes insufficient, and strength at high temperatures cannot be maintained at the desired level, thereby making this undesirable. If the composite ratio of Al exceeds 7.0 wt%, a large amount of a coarse γ phase referred to as the eutectic γ phase is formed, and this eutectic γ phase prevents solution treatment and makes it impossible to maintain strength at high temperatures at a high level, thereby making this undesirable.

Hf is an element that segregates at the grain boundary and improves strength at high temperatures by strengthening the grain boundary as a result of being segregated at the grain boundary between the γ phase and γ' phase. The composite ratio of Hf is preferably within the range of 0.01 wt% or more to 0.50 wt% or less, and most preferably 0.10 wt%. If the composite ratio of Hf is less than 0.01 wt%, the precipitated amount of the γ' phase becomes insufficient and

strength at high temperatures cannot be maintained at the desired level, thereby making this undesirable. However, the composite ratio of Hf may be within the range of 0 wt% or more to less than 0.01 wt%, if necessary. Furthermore, if the composite ratio of Hf exceeds 0.50 wt%, local melting is induced which results in the risk of decreased strength at high temperatures, thereby making this undesirable.

Co improves strength at high temperatures by increasing the solution limit at high temperatures relative to the matrix such as Al and Ta, and dispersing and precipitating a fine γ' phase by heat treatment. The composite ratio of Co is preferably within the range of 0.1 wt% or more to 9.9 wt% or less, and most preferably 5.8 wt%. If the composite ratio of Co is less than 0.1 wt%, the precipitated amount of the γ' phase becomes insufficient and the strength at high temperatures cannot be maintained, thereby making this undesirable. However, the composite ratio of Co may be within the range of 0 wt% or more to less than 0.1 wt%, if necessary. Furthermore, if the composite ratio of Co exceeds 9.9 wt%, the balance with other elements such as Al, Ta, Mo, W, Hf and Cr is disturbed resulting in the precipitation of harmful phases that cause a decrease in strength at high temperatures, thereby making this undesirable.

Re improves strength at high temperatures due to solution strengthening as a result of dissolving in the matrix in the form of the γ phase. On the other hand, if a large amount of Re is added, the harmful TCP phase precipitates at high temperatures, resulting in the risk of decreased strength at high temperatures. Thus, the composite ratio of Re is preferably within the range of 3.1 wt% or more to 8.0 wt% or less, and most preferably 4.9 wt%. If the composite ratio of Re is less than 3.1 wt%, solution strengthening of the γ phase becomes insufficient and strength at high temperatures cannot be maintained at the desired level, thereby making this undesirable. If the composite ratio of Re exceeds 8.0 wt%, the TCP phase precipitates at high temperatures and strength at high temperatures cannot be maintained at a high level, thereby making this undesirable.

Ru improves strength at high temperatures by inhibiting precipitation of the TCP phase. The composite ratio of Ru is preferably within the range of 4.1 wt% or more to 14.0 wt% or less. This ratio is more preferably within the range of 10.0 wt% or more to 14.0 wt% or less, or preferably within the range of 6.5 wt% or more to 14.0 wt% or less, and most preferably 5.0 wt%, 6.0 wt% or 7.0 wt%. If the composite ratio of Ru is less than 1.0 wt%, the TCP phase precipitates

at high temperatures and strength at high temperatures cannot be maintained at a high level, thereby making this undesirable. If the composite ratio of Ru is less than 4.1 wt%, strength at high temperatures decreases compared to the case when the composite ratio of Ru is 4.1 wt% or more. Furthermore, if the composite ratio of Ru exceeds 14.0 wt%, the ϵ phase precipitates and strength at high temperatures decreases which is also undesirable.

Particularly in the present invention, by adjusting the composite ratios of Al, Ta, Mo, W, Hf, Cr, Co and Ni to the optimum ratios, together with improving strength at high temperatures by setting the aftermentioned lattice misfit and dislocation networks of the alloy which are calculated from the lattice constant of the γ phase and the lattice constant of the γ' phase within their optimum ranges, and precipitation of the TCP phase can be inhibited by adding Ru. Furthermore, by adjusting the composite ratios of Al, Cr, Ta and Mo to the aforementioned ratios, the production cost for the alloy can be decreased. In addition, relative strength of the alloy can be increased and the lattice misfit and dislocation networks of the alloy can be adjusted to the optimum value.

In addition, in usage environments at a high temperature from 1273 K (1000°C) to 1373 K (1100°C), when the lattice constant of the crystals that compose the matrix in the form of the γ phase is taken to be a_1 , and the lattice constant of the crystals that compose the precipitation phase in the form of the γ' phase is taken to be a_2 , then the relationship between a_1 and a_2 is preferably such that $a_2 \leq 0.999a_1$. Namely, lattice constant a_2 of the crystals of the precipitation phase is preferably -0.1% or less lattice constant a_1 of the crystals of the matrix. Furthermore, it is more preferable that the lattice constant of the crystals of the precipitation phase a_2 is 0.9965 or less of the lattice constant of the crystals of the matrix a_1 . In this case, the above-described relationship between a_1 and a_2 becomes $a_2 \leq 0.9965a_1$. In the following descriptions, the percentage of the lattice constant a_2 relative to the lattice constant a_1 is called "lattice misfit".

In addition, in the case both of the lattice constants are in the above relationship, since the precipitation phase precipitates so as to extend continuously in the direction perpendicular to the direction of the load when the precipitation phase precipitates in the matrix due to heat treatment, creep strength can be enhanced without movement of dislocation defects in the alloy structure in the presence of stress.

In order to make the relationship between lattice constant a_1 and lattice constant a_2 such that

$a_2 \leq 0.999a_1$, the composition of the composite elements that compose the Ni-based single crystal super alloy is suitably adjusted.

FIG. 1 shows a relationship between the lattice misfit of the alloy and the time until the alloy demonstrates creep rupture (creep rupture life).

In FIG. 1, when the lattice misfit is approximately -0.35 or lower, the creep rupture life is approximately higher than the required value (the value shown by a dotted line in a vertical axis of the figure). Therefore, in the present invention, the preferable value of the lattice misfit is determined to -0.35 or lower. In order to maintain the lattice misfit to -0.35 or lower, the composition of Mo is maintained to a high level, and the composition of the other composite elements is suitably adjusted.

According to the above Ni-based super crystal super alloy, precipitation of the TCP phase, which causes decreased creep strength, during use at high temperatures is inhibited by addition of Ru. In addition, by setting the composite ratios of other composite elements to their optimum ranges, the lattice constant of the matrix (γ phase) and the lattice constant of the precipitation phase (γ' phase) can be made to have optimum values. As a result, creep strength at high temperatures can be improved.

Ti can be further included in the above Ni-based super crystal super alloy. The composite ratio of Ta is preferably within the range of 0 wt% or more to 2.0 wt% or less. If the composite ratio of Ti exceeds 2.0 wt%, the harmful phase precipitates and the strength at high temperatures cannot be maintained, thereby making this undesirable.

Furthermore, Nb can be further included in the above Ni-based super crystal super alloy. The composite ratio of Nb is preferably within the range of 0 wt% or more to 4.0 wt% or less. If the composite ratio of Nb exceeds 4.0 wt%, the harmful phase precipitates and the strength at high temperatures cannot be maintained, thereby making this undesirable.

Alternatively, strength at high temperatures can be improved by adjusting the total composite ratio of Ta, Nb and Ti ($Ta+Nb+Ti$) within the range of 4.0 wt% or more to 10.0 wt% or less.

Furthermore, in addition to the unavoidable impurities, B, C, Si, Y, La, Ce, V and Zr and the like can be included in the above Ni-based super crystal super alloy, for example. When the alloy

includes at least one of elements selected from B, C, Si, Y, La, Ce, V and Zr, the composite ratio of each element is preferably 0.05 wt% or less of B, 0.15 wt% or less of C, 0.1 wt% or less of Si, 0.1 wt% or less of Y, 0.1 wt% or less of La, 0.1 wt% or less of Ce, 1 wt% or less of V and 0.1 wt% or less of Zr. If the composite ratio of each element exceeds the above range, the harmful phase precipitates and the strength at high temperatures cannot be maintained, thereby making this undesirable.

Furthermore, in the above Ni-based single crystal super alloy, it is preferable that a dislocation space of the alloy is 40 nm or less. The reticulated dislocation (displacement of atoms which are connected as a line) in the alloy is called dislocation networks, and a space between adjacent reticulations is called "dislocation space". FIG. 2 shows a relationship between the dislocation space of the alloy and the time until the alloy demonstrates creep rupture (creep rupture life).

In FIG. 2, when the dislocation space is approximately 40 nm or lower, the creep rupture life is approximately higher than the required value (the value shown by a dotted line in a vertical axis of the figure). Therefore, in the present invention, the preferable value of the dislocation space is determined to 40 nm or lower. In order to maintain the dislocation space to 40 nm or lower, the composition of Mo is maintained to a high level, and the composition of the other composite elements is suitably adjusted.

FIG. 3 is a transmission electron microgram of the Ni-based single crystal super alloy showing an embodiment (aftermentioned embodiment 3) of the dislocation networks and dislocation space of the Ni-based single crystal super alloy of the present invention. As shown in FIG. 3, in case of the Ni-based single crystal super alloy of the present invention, the dislocation space is 40 nm or lower.

In addition, some of the conventional Ni-based single crystal super alloys may cause reverse partitioning, however, in Ni-based single crystal super alloy of the present invention does not cause reverse partitioning.

Embodiments

The effect of the present invention is shown using following embodiments.

Melts of various Ni-based single crystal super alloys were prepared using a vacuum melting

furnace, and alloy ingots were cast using the alloy melts. The composite ratio of each of the alloy ingots (reference examples 1-6, embodiments 1-14) is shown in Table 2.

Table 2

Sample (alloy name)	Elements (wt%)										
	Al	Ta	Nb	Mo	W	Re	Hf	Cr	Co	Ru	Ni
Reference Example 1	6.0	5.8		3.2	6.0	5.0	0.1	3.0	6.0	2.0	Rem
Reference Example 2	5.9	5.7		3.2	5.9	5.0	0.1	3.0	5.9	3.0	Rem
Reference Example 3	6.0	6.0		4.0	6.0	5.0	0.1	3.0	6.0	3.0	Rem
Reference Example 4	5.9	5.9		4.0	5.9	5.0	0.1	3.0	5.9	4.0	Rem
Reference Example 5	5.9	5.7		3.1	5.9	4.9	0.1	2.9	5.9	4.0	Rem
Reference Example 6	5.7	5.7		2.9	7.7	4.8	0.1	2.9	5.7	3.0	Rem
Embodiment 1	5.9	5.9		3.9	5.9	4.9	0.1	2.9	5.9	5.0	Rem
Embodiment 2	5.8	5.6		3.1	5.8	4.9	0.1	2.9	5.8	5.0	Rem
Embodiment 3	5.8	5.8		3.9	5.8	4.9	0.1	2.9	5.8	6.0	Rem
Embodiment 4	5.6	5.6		2.8	5.6	6.9	0.1	2.9	5.6	5.0	Rem
Embodiment 5	5.6	5.0	0.5	2.8	5.6	6.9	0.1	2.9	5.6	5.0	Rem
Embodiment 6	5.6	5.6	1.0	2.8	5.6	4.7	0.1	2.9	5.6	5.0	Rem
Embodiment 7	5.8	5.6		3.9	5.8	4.9	0.1	2.9	5.8	6.0	Rem
Embodiment 8	5.7	5.5	1.0	3.8	5.7	4.8	0.1	2.8	5.5	5.9	Rem
Embodiment 9	5.8	5.6		3.1	6.0	5.0	0.1	2.9	5.8	4.6	Rem
Embodiment 10	5.8	5.6		3.1	6.0	5.0	0.1	2.9	5.8	5.2	Rem
Embodiment 11	5.8	5.6		3.3	6.0	5.0	0.1	2.9	5.8	5.2	Rem
Embodiment 12	5.8	5.6		3.3	6.0	5.0	0.1	2.9	5.8	6.0	Rem
Embodiment 13	5.9	2.9	1.5	3.9	5.9	4.9	0.1	2.9	5.9	6.1	Rem
Embodiment 14	5.7	5.52		3.1	5.7	4.8	0.1	2.9	5.7	7.0	Rem

Next, solution treatment and aging treatment were performed on the alloy ingots followed by observation of the state of the alloy structure with a scanning electron microscope (SEM).

Solution treatment consisted of holding for 1 hour at 1573K (1300°C) followed by heating to 1613K (1340°C) and holding for 5 hours. In addition, aging treatment consisted of consecutively performing primary aging treatment consisting of holding for 4 hours at 1273K-1423K (1000°C -1150°C) and secondary aging treatment consisting of holding for 20 hours at 1143K (870°C).

As a result, a TCP phase was unable to be confirmed in the structure of each sample.

Next, a creep test was performed on each sample that underwent solution treatment and aging treatment. The creep test consisted of measuring the time until each sample (reference examples 1-6 and embodiments 1-14) demonstrated creep rupture as the sample life under each of the temperature and stress conditions shown in Table 3. Furthermore, the value of the lattice misfit of each sample was also measured, and the result thereof is disclosed in Table 3. In addition, the value of the lattice misfit of each of the conventional alloys shown in Table 1 (comparative examples 1-5) was also measured, and the result thereof is disclosed in Table 4.

Table 3

Sample (alloy name)	Creep test conditions/rupture life (h)		Lattice Misfit
	1273K (1000°C) 245 MPa	1373K (1100°C) 137 MPa	
Reference Example 1	209.35	105.67	-0.39
Reference Example 2	283.20	158.75	-0.40
Reference Example 3	219.37	135.85	-0.56
Reference Example 4	274.38	153.15	-0.58
Reference Example 5	328.00	487.75	-0.58
Reference Example 6		203.15	-0.41
Embodiment 1	5.09.95	32.6.50	-0.60
Embodiment 2	420.60	753.95	-0.42
Embodiment 3		1062.50	-0.62
Embodiment 4		966.00	-0.44
Embodiment 5		1256.00	-0.48
Embodiment 6		400.00	-0.45
Embodiment 7		1254.00	-0.60
Embodiment 8		682.00	-0.63
Embodiment 9		550.00	-0.42
Embodiment 10		658.50	-0.45
Embodiment 11		622.00	-0.48
Embodiment 12		683.50	-0.51
Embodiment 13	412.7	766.35	-0.62
Embodiment 14		1524.00	-0.45

Table 4

Sample (alloy name)	Lattice Misfit
Comparative Example 1 (CMSX-2)	-0.26
Comparative Example 2 (CMSX-4)	-0.14
Comparative Example 3 (Rene N6)	-0.22
Comparative Example 4 (CMSX-10K)	-0.14
Comparative Example 5 (3B)	-0.25

As is clear from Table 3, the samples of the reference examples 1-6 and embodiments 1-14

were determined to have high strength even under high temperature conditions of 1273K (1000°C). In particular, reference example 5 having a composition of 4.0 wt% of Ru, embodiments 1, 2, 4, 9, 10 and 11 having a composition approximately 5.0 wt% of Ru, embodiments 3, 12 and 13 having a composition of 6.0 wt% of Ru, and embodiment 14 having a composition of 7.0 wt% of Ru, were determined to have high strength at high temperature.

Furthermore, as is clear from Tables 3 and 4, the lattice misfit of comparative examples were -0.35 and more, whereas those of reference examples 1-6 and embodiments 1-14 were -0.35 or less.

In addition, the creep rupture characteristics (withstand temperature) were compared for the alloys of the prior art shown in Table 1 (Comparative Examples 1 through 5) and the sample shown in Table 2 (reference examples 1-6 and embodiments 1-14). The result thereof is disclosed in Table 5. Creep rupture characteristics were determined either as a result of measuring the temperature until the sample ruptured under conditions of applying stress of 137 MPa for 1000 hours, or converting the rupture temperature of the sample under those conditions.

Table 5

Sample (alloy name)	Withstand temperature (°C)
Reference Example 1	1315K (1042°C)
Reference Example 2	1325K (1052°C)
Reference Example 3	1321K (1048°C)
Reference Example 4	1324K (1051°C)
Reference Example 5	1354K (1081°C)
Reference Example 6	1332K (1059°C)
Embodiment 1	1344K (1071°C)
Embodiment 2	1366K (1093°C)
Embodiment 3	1375K (1102°C)
Embodiment 4	1372K (1099°C)
Embodiment 5	1379K (1106°C)
Embodiment 6	1379K (1106°C)
Embodiment 7	1379K (1106°C)
Embodiment 8	1363K (1090°C)
Embodiment 9	1358K (1085°C)
Embodiment 10	1362K (1089°C)
Embodiment 11	1361K (1088°C)
Embodiment 12	1363K (1090°C)
Embodiment 13	1366K (1093°C)
Embodiment 14	1384K (1111°C)
Comparative Example 1 (CMSX-2)	1289K (1016°C)
Comparative Example 2 (CMSX-4)	1306K (1033°C)
Comparative Example 3 (ReneN6)	1320K (1047°C)
Comparative Example 4 (CMSX-10K)	1345K (1072°C)
Comparative Example 5 (3B)	1353K (1080°C)

(Converted to 137 MPa, 1000 hours)

As is clear from Table 5, the samples of reference examples 1-6 and embodiments 1-14 were determined to have a high withstand temperature (1356K (1083°C)) equal to or greater than the alloys of the prior art (comparative Examples 1-5). In particular, samples of reference examples 1-6 and embodiments 1-14 were determined to have a high withstand temperature (embodiment 1: 1344K (1071°C), embodiment 2: 1366K (1093°C), embodiment 3: 1375K (1102°C), embodiment 4: 1372K (1099°C), embodiment 5: 1379K (1106°C), embodiment 6: 1379K (1106°C), embodiment 7: 1379K (1106°C), embodiment 8: 1363K (1090°C), embodiment 9: 1358K (1085°C), embodiment 10: 1362K (1089°C), embodiment 11: 1361K (1088°C),

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embodiment 12: 1363K (1090°C), embodiment 13: 1366K (1093°C) and embodiment 14: 1384K (1111°C)).

Thus, this alloy has a higher heat resistance temperature than Ni-based single crystal super alloys of the prior art, and was determined to have high strength even at high temperatures.

Furthermore, in the Ni-based single crystal super alloy, if the composite ratio of Ru excessively increases, the ϵ phase precipitates and strength at high temperatures decreases.

Therefore, the composite ratio of Ru is preferably be determined to a range so as to keep the balance against the composition of the other composite elements is suitably adjusted (4.1 wt% or more to 14.0 wt% or less, for example).